

Formation of Protective Iron Carbonate Films on Steel Pipeline

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Motivations

- ❖ CO₂ corrosion (sweet corrosion) is a significant problem for steel pipelines in the oil and gas production industry
- ❖ Sweet corrosion is caused by the dissolution of CO₂ in co-produced water
- ❖ Two opposing effects: dissolution accelerator (via the formation of a carbonic acid) and corrosion inhibitor (via the formation of a siderite film)
- ❖ Protective nature of the film depends on the conditions of its formation

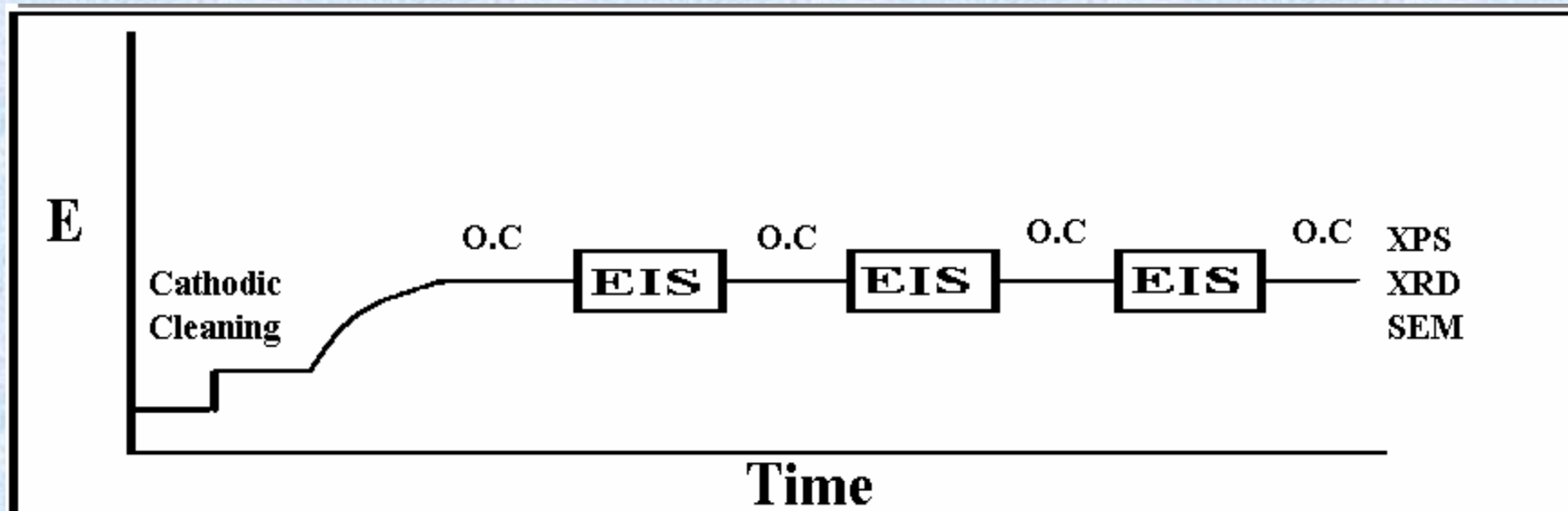
Experimental

Electrode: carbon steel cut from Edson mainline loop (from NRTC)

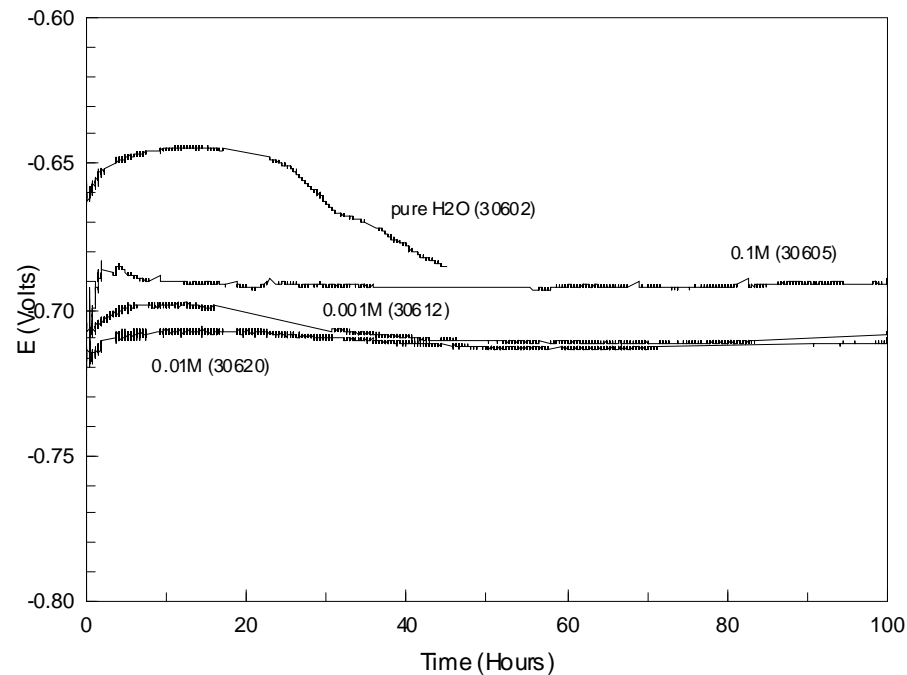
Solution: 0.1, 0.01, 0.001 mol/L NaClO₄ (+NaOH for pH adjustment)

Setup: two-side-arm cell deaerated with CO₂ at atmospheric pressure

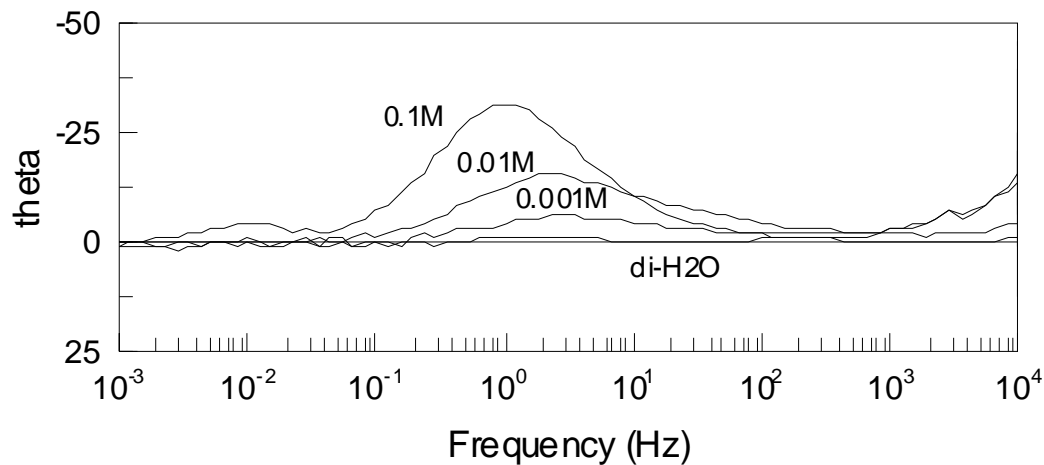
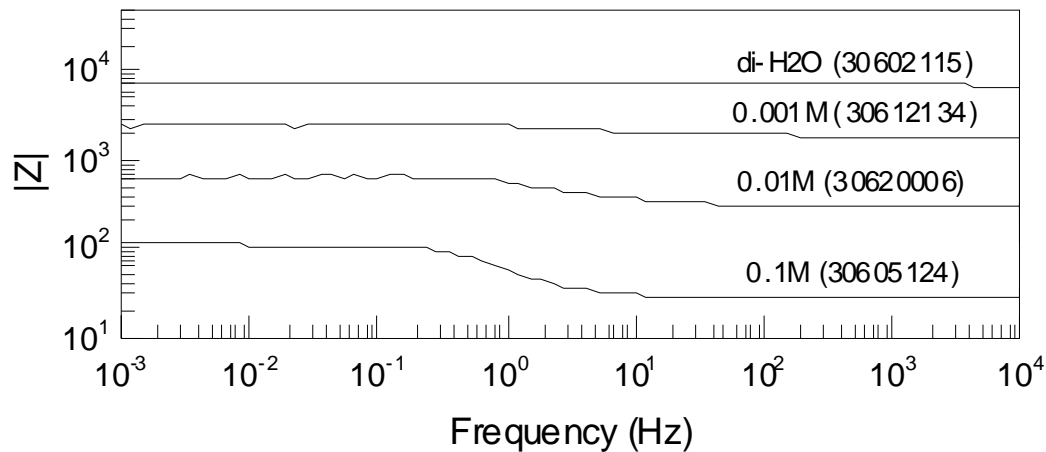
Procedures:



Is a supporting NaClO_4 electrolyte necessary?

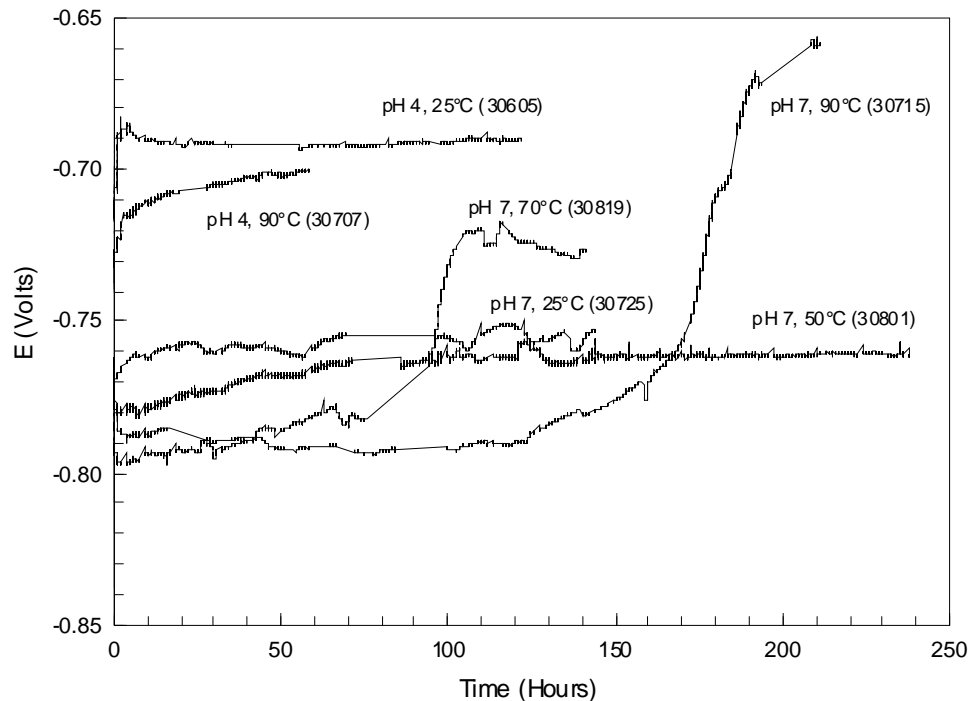


Solution	0.1M NaClO_4	0.01M NaClO_4	0.001M NaClO_4	Deionized H_2O
Initial pH	3.755	3.756	3.840	3.796
Final pH	4.820	4.484	4.718	4.309
R_s (Ω)	28	290	1735	6192



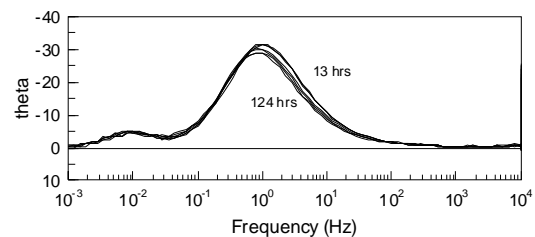
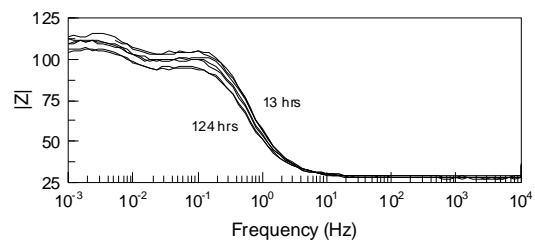
- ❖ The impedance magnitude increases and the maximum phase angle decreases with decreased concentrations
- ❖ EIS is dominated by R_s and little interfacial information is revealed in dilute solutions ($< 0.01\text{M}$)

- ❖ $\text{pH} \uparrow, E_{\text{corr}} \downarrow$
- ❖ $T \uparrow, E_{\text{corr}} \downarrow$
- ❖ $E^e_{\text{C}} < E_{\text{corr}} < E^e_{\text{A}}$
- ❖ The sudden jump in E_{corr} in the neutral solutions at 70 and 90°C may indicate changes in the balance of corrosion kinetics

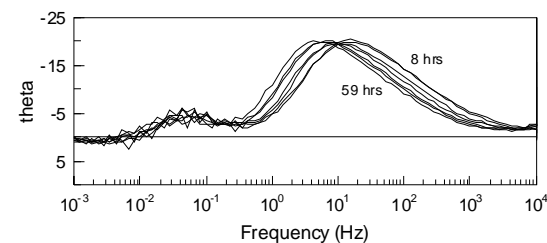
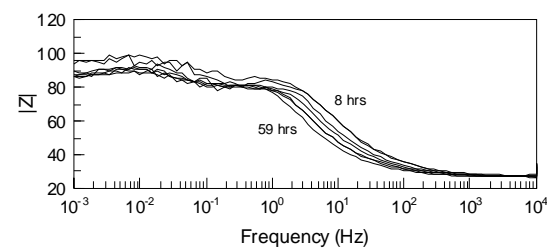


Conditions	$E^e_{\text{H}^+ \text{H}}$	$E^e_{\text{Fe} \text{Fe}^{++}}$	E_{corr}
pH = 3.755 – 4.820, 25°C	-0.526	-0.740	-0.691 ± 0.003
pH = 3.555 – 5.209, 90°C	-0.616	-0.781	-0.706 ± 0.006
pH = 7.066 – 6.974, 25°C	-0.653	-0.867	-0.758 ± 0.003
pH = 6.991 – 7.017, 50°C	-0.690	-0.886	-0.765 ± 0.005
pH = 7.062 – 7.658, 70°C	-0.762	-0.942	$-0.788 \pm 0.005 (\leq 72\text{h})$
pH = 7.034 – 7.418, 90°C	-0.774	-0.940	$-0.790 \pm 0.003 (\leq 124\text{h})$

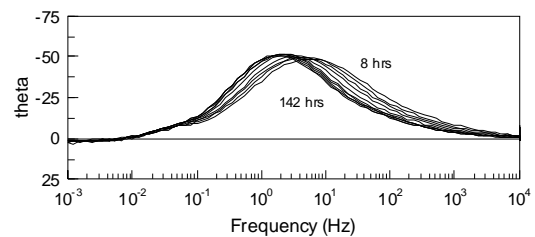
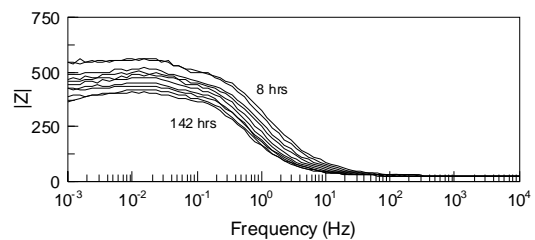
pH 4, 25°C (30605)



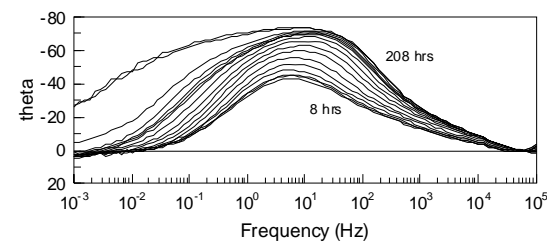
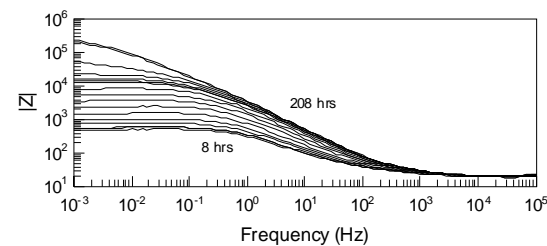
pH 4, 90°C (30707)



pH 7, 25°C (30725)



pH 7, 90°C (30715)



Methods to calculate polarization resistance R_p

Extrapolation

$$R_p = \lim_{\omega \rightarrow 0} |Z| - \lim_{\omega \rightarrow \infty} |Z|$$

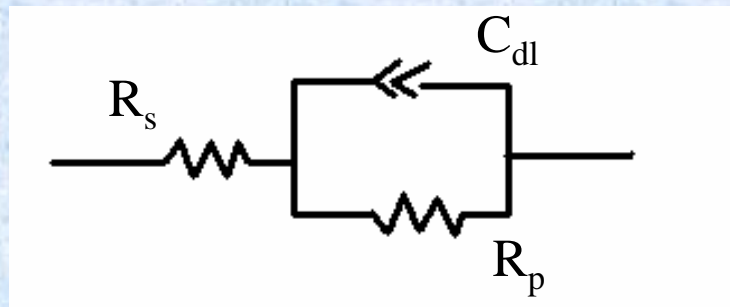
**Tangential
approximation**

$$R_p \cong 2|Z_m| \tan \phi_{\max}$$

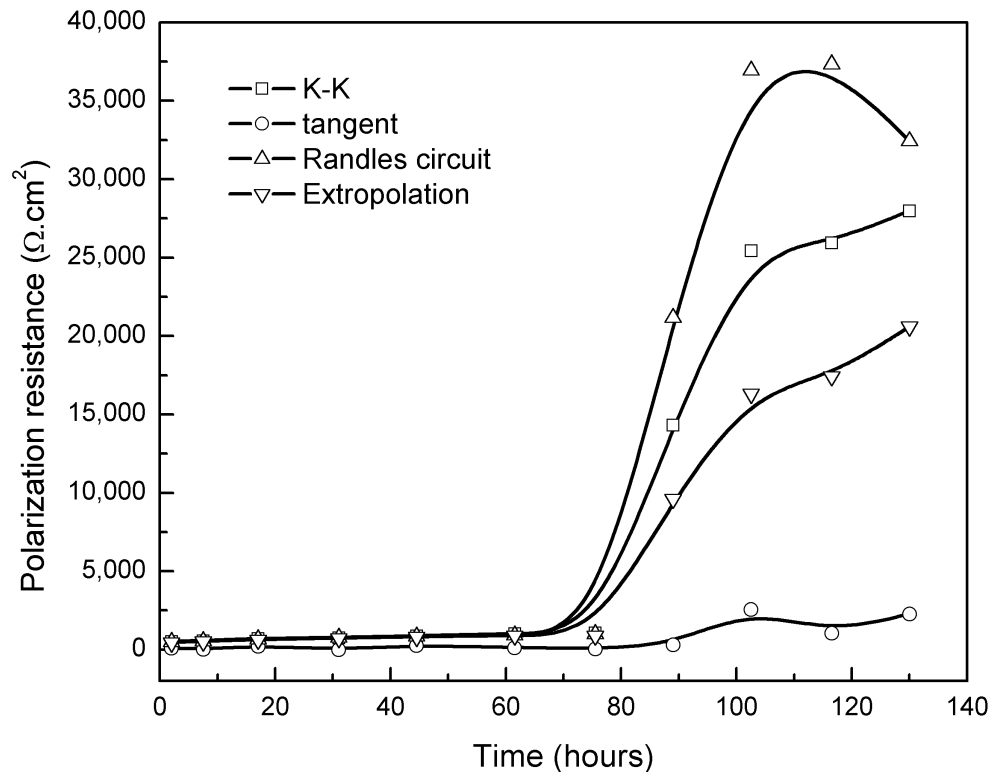
**Kramers-Kronig
transform**

$$R_p \cong 2.932 \left| \int_{\log \omega_m}^{\infty} \text{Im}[Z(\omega)] d \log \omega \right|$$

Equivalent circuit



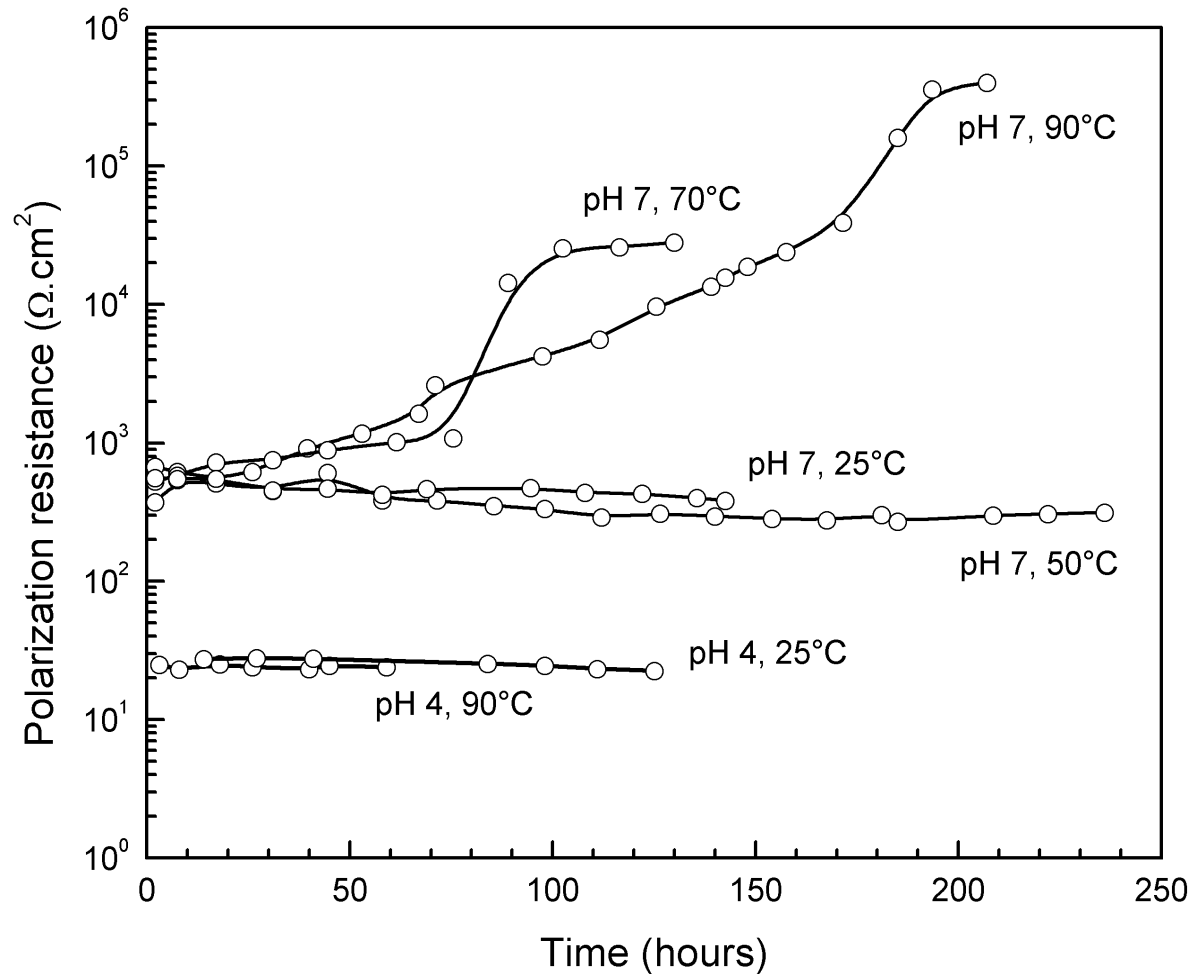
R_p calculated from the same set of EIS



(b)

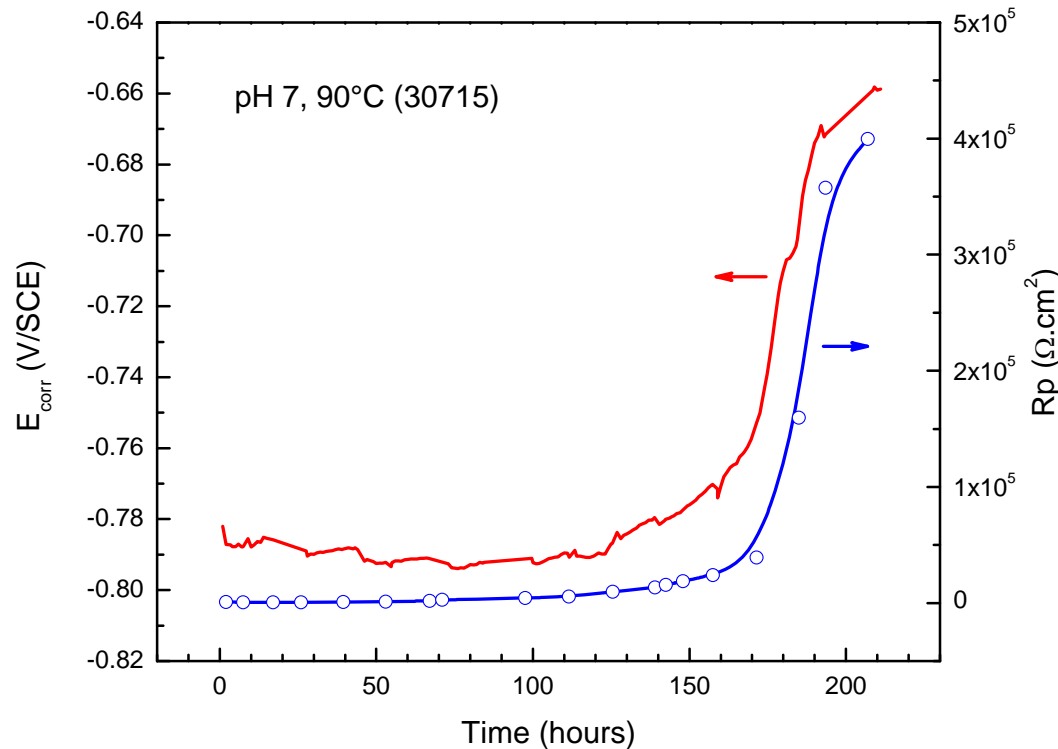
- ❖ Too low R_p values from Tangential approximation
- ❖ R_p given by K-K approximation in between those by the extrapolation and equivalent circuit

R_p calculated by K-K for various conditions

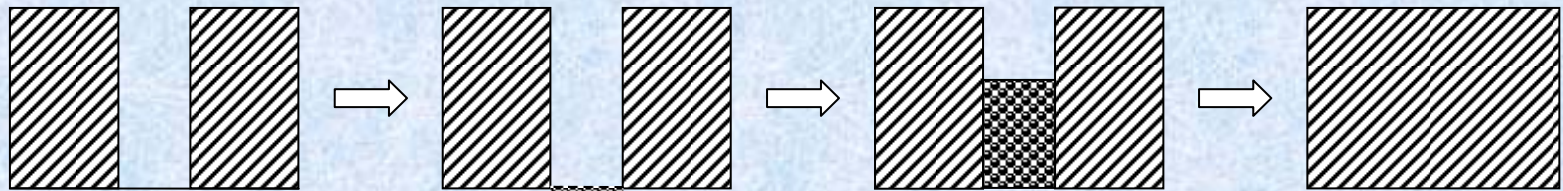


Formation of a protective film

- ❖ The abrupt increase in R_p indicates the formation of a protective film that mitigates corrosion
- ❖ The increase in E_{corr} at the same time could attribute to switching the galvanic couplings

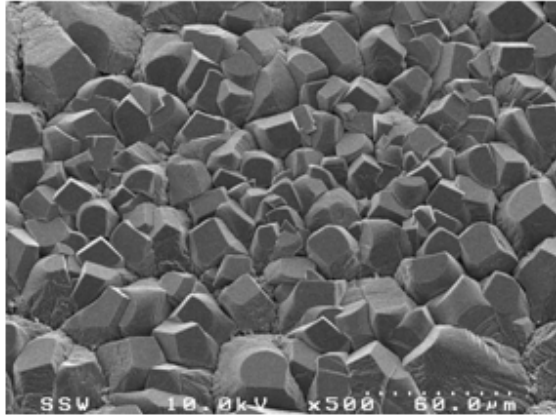


Formation mechanism of protective films

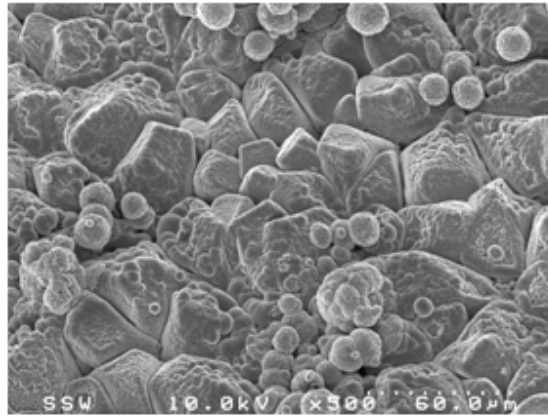


- ❖ Precipitation of FeCO_3 would first form a porous film, and R_p is dominated by the low resistances in pores
- ❖ Precipitation then more likely occurs at the bottom of the pores
- ❖ The turning point in R_p could be the indication of virtually sealing film porosity. Then R_p becomes film resistance dominated
- ❖ The sealing layer might be very thin at first, but will grow until the whole length of pores are filled

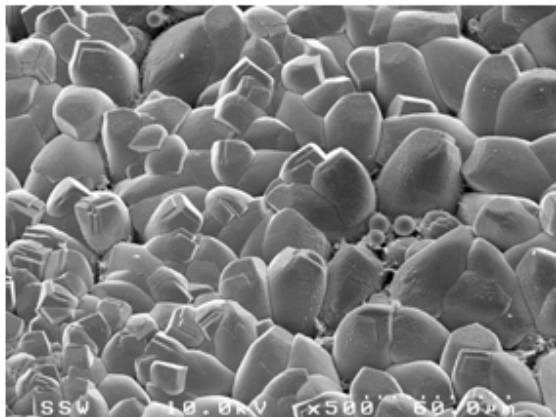
SEM images after immersion



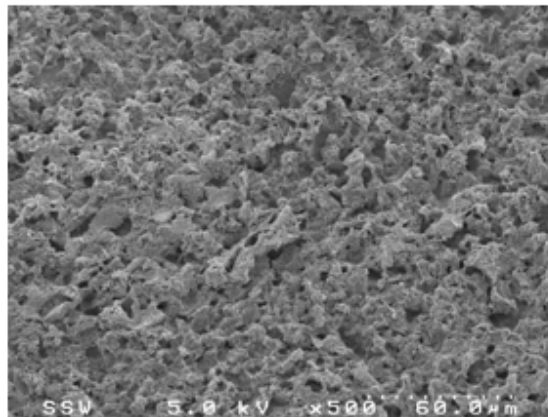
(a)



(b)



(c)



(d)

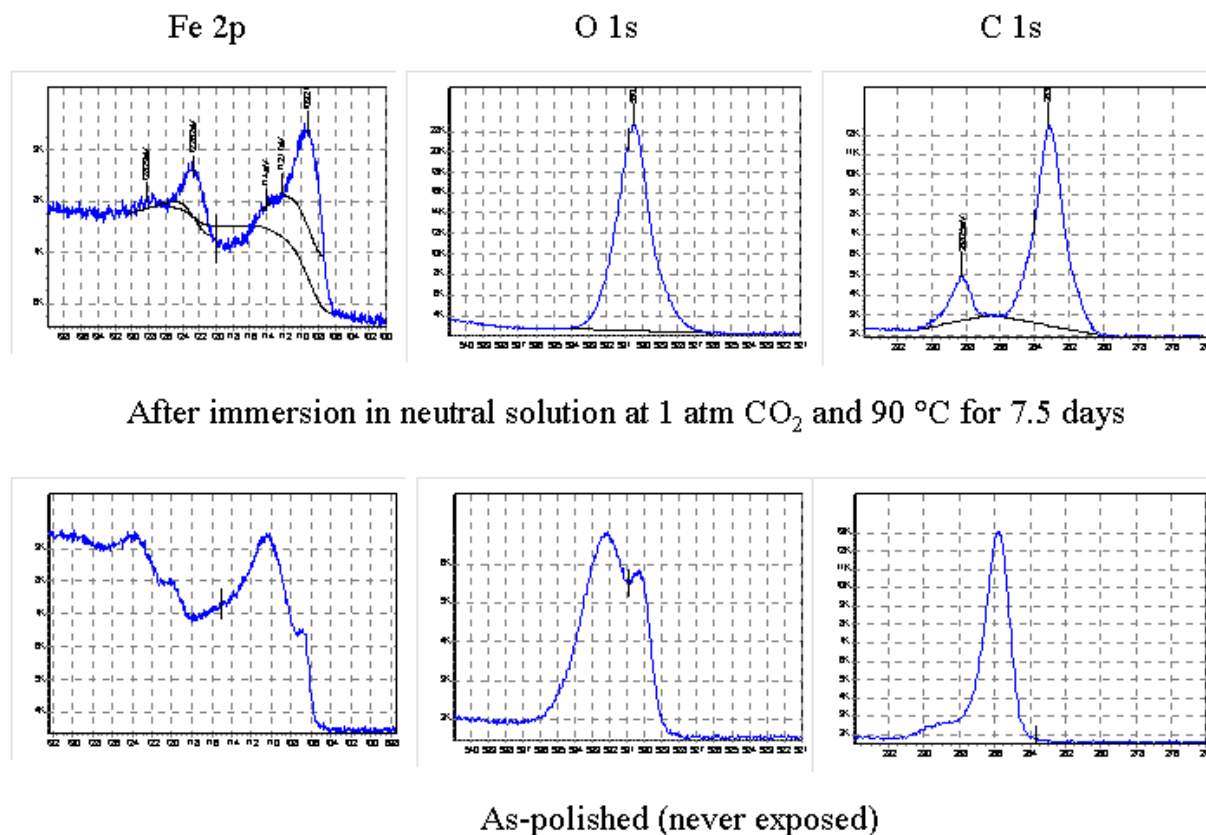
a. pH~7,90°C

b. pH~7,70°C

c. pH~7,50°C

d. pH~4,90°C

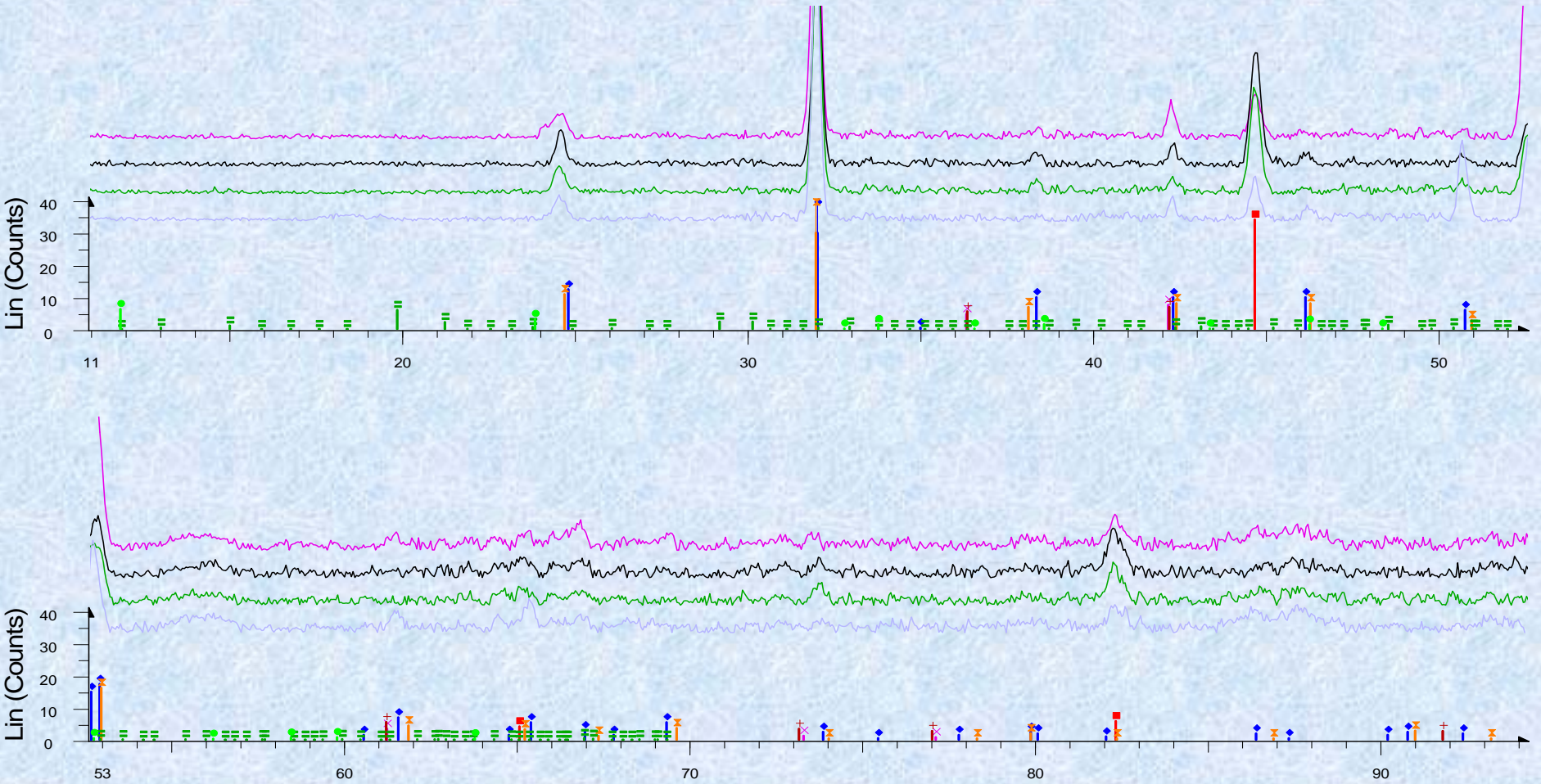
XPS confirmed
siderite film on
the surface of
the immersed
specimen



Peak	C1s	O1s	Fe2p _{3/2}	Fe2p _{3/2} satellite	Fe2p _{1/2}
This study	289.5	531.9	710.7	715.4	724.0
Siderite*	289.4	531.9	710.2	714.9	723.7

* J. K. Heuer and J. F. Stubbins, Corrosion Science, 41 (1999), 1231-1243

XRD Analysis



2-Theta - Scale

- | | |
|--|---|
| Y + 20.0 mm - File: ZackFeCO3_CO2_01 [001].raw | 03-0746 (D) - Siderite - FeCO3 |
| Y + 25.0 mm - File: ZackFeCO3_CO2_02 [001].raw | 74-1880 (C) - Wuestite - Fe.9536O |
| Y + 30.0 mm - File: ZackFeCO3_CO2_03 [001].raw | 46-1312 (N) - Wuestite - FeO |
| Y + 35.0 mm - File: ZackFeCO3_CO2_04 [001].raw | 76-0956 (C) - Magnetite - Fe3O4 |
| 87-0721 (C) - Iron - Fe | 50-1380 (N) - Iron Carbonate Hydroxide Hydrate - Fe6(OH)12CO3.2 |
| 29-0696 (*) - Siderite - FeCO3 | |

Conclusions

- ❖ A protective siderite film is formed in neutral solutions and temperatures higher than 70°C
- ❖ The transitions in R_p and E_{corr} indicate the formation of a protective film
- ❖ Precipitates of FeCO_3 would first form a porous film where corrosion continues at the base of pores. The film will become protective when the pores are sealed by thin FeCO_3 layers at the bases, since then corrosion has to proceed through the passive layer